Sensor Fusion and Optimal Platform Trajectory Planning for Ground Target Localization with Terrain Uncertainty and Measurement Biases

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- 3-D ground target localization with biased angle-only sensor.
- Two key sources of uncertainties:
 - Measurement bias, i.e. bias in the elevation and bearing angles.
 - Terrain uncertainty.
- Ground target can be:
 - Stationary.
 - Moving with a nearly constant velocity (CV).

Terrain Uncertainty



- How to make the 3-D localization problem observable?
 - The target height from the sea level is available.
 - Height information is obtained from a Digital Terrain Elevation Database (DTED).
- Height information obtained from DTED has uncertainty.
- Neglecting terrain uncertainty leads to:
 - Localization error.
 - Optimistic performance bounds.





Localization using Angle-only Sensor¹



- Tracking a ground target in 3-D using angle-only airborne sensor.
- Ground target height from the sea level is assumed to be known with terrain uncertainty.
 - Sources of uncertainties: terrain uncertainty and measurement bias.
- Bias estimation using a target of opportunity.
 - Optimal number of target of opportunity.
 - Optimal sensor trajectory.
- Target localization using bias compensated non-linear filtering.
- Evaluation of biased posterior Cramer Rao Lower Bound (PCRLB) and estimator performance evaluation.

¹D. Mitra, A. Balachandran, R. Tharmarasa, "Ground Target Tracking Using an Airborne Angle-Only Sensor with Terrain Uncertainty and Sensor Biases," Sensors, 22, no. 2:509, January 2022, pp. 1-26.



• Challenges:

- Presence of measurement bias causes delay in error convergence.
- Estimation accuracy is low.
- Proposed solution:
 - Range sensor addition to improve localization accuracy.
 - Error convergence is attained faster.
 - Platform trajectory optimization for estimation.
 - Ground target localization while handling biases.
 - Bias compensation.
 - Bias estimation.

Problem Overview



- Localizing a ground target using two airborne sensor platforms.
 - Ground target has terrain uncertainty.
 - Platform 1 contains biased angle-only sensors.
 - Platform 2 contains unbiased range sensor.
- Optimal platform trajectory based on performance bound.





Measurement Model (for Platform 1)

Biased angle-only measurements θ_k ∈ [-π, π] and γ_k ∈ [-π/2, π/2].
From 3-D geometry,

$$\theta_k^{\text{true}} = \tan^{-1} \left(y_k^t - y_k^{p1}, x_k^t - x_k^{p1} \right)$$
 (1)

$$\gamma_k^{\text{true}} = \tan^{-1} \left(\sqrt{\left(x_k^t - x_k^{p1} \right)^2 + \left(y_k^t - y_k^{p1} \right)^2}, z_k^t - z_k^{p1} \right)$$
 (2)

- True height of the ground target from the sea level is z^t_k.
- Assumed height containing terrain uncertainty $z_g = z_1^t + \tilde{z}^t$.
 - Error associated to terrain uncertainty $\tilde{z}^t \sim \mathcal{N}(\tilde{z}^t; 0, \sigma_{z^t}^2)$.
- Measurement model for platform 1,

$$\mathbf{z}_{k} = \mathbf{h}_{a}(\mathbf{x}_{k}^{t}, \mathbf{x}_{k}^{p1}) + \mathbf{b}_{k} + \mathbf{w}_{k}$$
(3)

• Bias vector
$$\mathbf{b}_k = [\theta_{b_k}, \gamma_{b_k}]$$
.
• $\mathbf{h}_a(\mathbf{x}_k^t, \mathbf{x}_k^{p1}) = [\theta_k^{\text{true}}, \gamma_k^{\text{true}}]^T$.
• Measurement noise $\mathbf{w}_k \sim \mathcal{N}(\mathbf{w}_k; 0, \mathbf{R}_k)$, where $\mathbf{R}_k = \text{diag}(\sigma_{\theta}^2, \sigma_{\gamma}^2)$.



• Unbiased range measurements,

$$r_k = \sqrt{(x_k^t - x_k^{p2})^2 + (y_k^t - y_k^{p2})^2 + (z_k^t - z_k^{p2})^2}$$
(4)

• Measurement model for platform 2,

$$\mathbf{z}_k^r = \mathbf{h}_r(\mathbf{x}_k^t, \mathbf{x}_k^{p2}) + \mathbf{w}_k^r$$
(5)

• $\mathbf{h}_r(\mathbf{x}_k^t, \mathbf{x}_k^{p2}) = [r_k].$

- Measurement noise \mathbf{w}_k^r is a zero-mean Gaussian with variance $\sigma_{r_k}^2$.
- Range measurements might not be available for all time-steps.

• Bias compensated measurements

$$\mathbf{z}_{k}^{c} = \mathbf{h}_{a}(\mathbf{x}_{k}^{t}, \mathbf{x}_{k}^{p1}) + \mathbf{b}_{k} - \mathbf{b}_{k}^{\mathsf{prior}} + \mathbf{w}_{k}^{c}$$
(6)

- Bias prior $\mathbf{b}_{k}^{\text{prior}} = [\theta_{b_{k}}^{\text{prior}}, \gamma_{b_{k}}^{\text{prior}}].$
- Measurement noise $\mathbf{w}_k^c \sim \mathcal{N}(\mathbf{w}_k^c; 0, \mathbf{R}_k^c)$.
- Bias compensated covariance $\mathbf{R}_{k}^{c} = \operatorname{diag}((\sigma_{\theta}^{2} + \sigma_{\theta_{b_{k}}^{\text{prior}}}^{2}), (\sigma_{\gamma}^{2} + \sigma_{\gamma_{b_{k}}^{\text{prior}}}^{2})).$
- Considering terrain uncertainty (only for initialization) $\mathbf{R}_{1} = \operatorname{diag}\left(\sigma_{z^{t}}^{2}, \left(\sigma_{\theta_{k}}^{2} + \sigma_{\theta_{b_{1}}}^{2}\right), \left(\sigma_{\gamma_{k}}^{2} + \sigma_{\gamma_{b_{1}}}^{2}\right)\right)$
- Unscented Kalman Filter (UKF) is used for non-linear filtering with zero point initialization.







- No bias compensation is performed.
- Bias states are stacked with the target state.
 - Joint state initialization as $\mathbf{x}_1 = [x_1, 0, y_1, 0, z_g, \theta_{b_k}^{\text{prior}}, \gamma_{b_k}^{\text{prior}}].$
 - For stationary target $\mathbf{x}_1 = [x_1, y_1, z_g, \theta_{b_k}^{\text{prior}}, \gamma_{b_k}^{\text{prior}}].$
 - $\theta_{b_k}^{\text{prior}}$ and $\gamma_{b_k}^{\text{prior}}$ can be zero.
- UKF is used for non-linear filtering.
- Information on terrain uncertainty not used after initialization.

Performance Bound

Posterior Cramer Rao Lower Bound (PCRLB) is used.
With Z_K = [z₁, z₂, ..., z_K],

$$\mathbf{C}_{k} = \mathbb{E}\left[(\hat{\mathbf{x}}_{k}^{t}(\mathbf{z}_{k}) - \mathbf{x}_{k}^{t}) (\hat{\mathbf{x}}_{k}^{t}(\mathbf{z}_{k}) - \mathbf{x}_{k}^{t})^{T} \right] \ge \mathbf{J}_{k}^{-1}$$
(7)

• Fisher Information Matrix (FIM) or J_k,

$$\mathbf{J}_{k+1} = \left(\mathbf{F}_k \mathbf{J}_k^{-1} \mathbf{F}_k^T + \mathbf{Q}_k\right)^{-1} + \mathbf{J}_z(k+1)$$
(8)

- Measurement contribution $\mathbf{J}_{z}(k) = \mathbb{E}\Big[q_{k}\mathbf{H}_{k}^{T}\mathbf{R}_{k}^{-1}\mathbf{H}_{k}\Big].$
- For angle-only sensors $\mathbf{H}_k = \frac{\partial \mathbf{h}_a(\mathbf{x}_k^t, \mathbf{x}_k^{p_1})}{\mathbf{x}_k^t}$.
- For range-only sensor $\mathbf{H}_k = \frac{\partial \mathbf{h}_r(\mathbf{x}_k^t, \mathbf{x}_k^{p^2})}{\mathbf{x}_k^t}$
- For range and angle measurements $\mathbf{J}_z(k) = \mathbf{J}_z^a(k) + \mathbf{J}_z^r(k)$.
 - $\mathbf{J}_z(k) = \mathbf{J}_z^a(k)$ or $\mathbf{J}_z(k) = \mathbf{J}_z^r(k)$, based on the availability of the sensor.



Range Sensor Fusion (1)





(a) Localization affected by θ_{b_k}

(b) Range sensor fusion with θ_{b_k}

Figure: Target state and the localization estimates in presence of biases in the angle measurements with $\mu = 0$.

Range Sensor Fusion (2)





(a) Localization affected by γ_{b_k}

(b) Range sensor fusion with γ_{b_k}

Figure: Target state and the localization estimates in presence of biases in the angle measurements with $\mu = 0$.

Optimal Trajectory Planning (1)





(a) Range sensor fusion with γ_{b_k}



(b) Range sensor fusion with θ_{b_k}

Figure: x-y plane projection of stationary target state and the localization estimates with sensor fusion and $\mu > 0$.

Optimal Trajectory Planning (1)

- Goal: Finding optimal μ by optimizing PCRLB.
- Measurement contribution of the FIM,

$$\mathbf{J}_{z}(k) = \mathbf{J}_{z}^{a}(k) + \mathbf{J}_{z}^{r}(k)$$
(9)

- Sampling rate of the range sensor might be different from the angle-only sensors.
- $\mathbf{J}_{z}^{r}(k)$ might not be available for all the time-steps.
- The optimization problem is formulated as,

$$\arg\min_{\mu} \sum_{k=1}^{K} \operatorname{Tr}[\mathbf{J}_{k}^{-1}]$$
(10)
s.t. $\mu \in [0, 360^{\circ})$

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- The bias in the angle-only measurements are smaller \rightarrow Choose $\mu = 0$.
- For larger bias in the angle-only measurements → Increase separation between the platforms.

Simulation Results (1)





Figure: Comparison of the RMSE of the proposed approach with an approach that ignores the terrain uncertainty, when the $\sigma_{z^t} = 30$ m.

Simulation Results (2)





Figure: Ground target localization errors for various terrain uncertainties using range sensor fusion for the platform separation angle $\mu = 0^{\circ}$.

• Higher terrain uncertainty leads to higher localization error.

Simulation Results (3)





Figure: Comparison of errors in target state localization using range sensor fusion for various degrees of separations between airborne platforms.

• $\mu = 90^{\circ}$ leads to faster reduction in RMSE for localization.

Simulation Results (4)



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(a) Bearing bias estimation errors

(b) Elevation bias estimation errors

Figure: Comparison of bias estimation errors for various angles of separation.

- $\mu = 90^{\circ}$ is optimal for bearing bias estimation.
- $\mu = 0^{\circ}$ is optimal for elevation bias estimation.

Simulation Results (5)





Figure: Comparison of ground target localization error for various μ with $\sigma_{\theta_b} = 1^\circ$, $\sigma_{\gamma_b} = 1^\circ$ and $\sigma_{z^t} = 30$ m.

- Impact of the higher μ on reducing localization error fades away for small biases.
- Terrain uncertainty primarily impacts localization accuracy \rightarrow Increasing μ has no effect in reducing RMSE.

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Conclusions



- Localization of a ground target using,
 - Biased angle-only sensors.
 - Additional range sensor —> Improves error convergence.
- Uncertainties present \longrightarrow
 - Measurement bias uncertainty.
 - Terrain uncertainty.
- Proposed localization approaches \longrightarrow
 - Use bias compensated measurements with inflated initial covariance.
 - Joint estimation of the bias and the target states. (Recommended method, if time is not a constraint)
- PCRLB based optimal platform trajectory planning \longrightarrow
 - Choose 90° separation for higher bearing biases.
 - Choose 0° separation for lower bearing biases.

Backup Slides

System Model



- Ground target state $\mathbf{x}_k^t = [x_k^t, \dot{x}_k^t, y_k^t, \dot{y}_k^t, z_k^t].$
- State evolution of ground target,

$$\mathbf{x}_{k+1}^t = \mathbf{F}_k \mathbf{x}_k^t + \mathbf{G}_k \mathbf{v}_k \tag{11}$$

- Process noise $\mathbf{v}_k \sim \mathcal{N}(\mathbf{v}_k; 0, \sigma_v^2)$.
- For a stationary ground target $\dot{x}_k^t = \dot{y}_k^t = 0$ and $\mathbf{F}_k = \mathbf{I}$.
- Platform 1 and 2 with states $\mathbf{x}_k^{p1} = [x_k^{p1}, \dot{x}_k^{p1}, y_k^{p1}, \dot{y}_k^{p1}, z_k^{p1}]$ and $\mathbf{x}_k^{p2} = [x_k^{p2}, \dot{x}_k^{p2}, y_k^{p2}, \dot{y}_k^{p2}, z_k^{p2}]$.
 - Platforms follow a 'coordinated turn model'.
 - Ground target remains at the centre of the circle.
 - Circle radius *R* and the constant speed *v* are known a-priori.
 - Turn rate $\omega = \frac{v}{R}$ rad/s.
 - Angle of separation is μ .



Platform radius (R)	3000 m
Platform speed (v)	50 m/s
Platform height (z_1^{p1})	700 m
Standard deviation of terrain uncertainty (σ_{z^t})	30 m
Range measurement standard deviation (σ_{r_k})	5 m
Bearing measurement standard deviation (σ_{θ_k})	0.4°
Elevation measurement standard deviation (σ_{γ_k})	0.2°
Sampling time of the angle-only sensor (T_1)	1 s
Sampling time of the range sensor (T_2)	5 s
Mean bearing bias (θ_{b_k})	0°
Bearing bias standard deviation $(\sigma_{\theta_{b_k}})$	5°
Mean elevation bias (γ_{b_k})	0°
Elevation bias standard deviation ($\sigma_{\gamma_{b_k}}$)	1°

Simulation Results (Backup)





Figure: Target own-ship geometry along with the estimates for the airborne platform separation angle $\mu = 0^{\circ}$.





Figure: Ground target localization error using range sensor fusion for the platform separation angle $\mu = 0^{\circ}$ and $\sigma_{z^t} = 30$ m.

Simulation Results (Backup)





Figure: Bias estimation errors for the airborne platform separation angle $\mu = 0^{\circ}$.